organic compounds

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N-(2-Fluorobenzoyl)-N',N"-bis(4-methylphenyl)phosphoric triamide

Mehrdad Pourayoubi,^a* Atekeh Tarahhomi,^a Arnold L. Rheingold^b and James A. Golen^b

^aDepartment of Chemistry, Ferdowsi University of Mashhad, Mashhad 91779, Iran, and ^bDepartment of Chemistry, University of California, San Diego, 9500 Gilman Drive, La Jolla, CA 92093, USA Correspondence e-mail: mehrdad_pourayoubi@yahoo.com

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Key indicators: single-crystal X-ray study; T = 100 K; mean σ (C–C) = 0.003 Å; R factor = 0.046; wR factor = 0.127; data-to-parameter ratio = 17.2.

The P atom in the title compound, $C_{21}H_{21}FN_3O_2P$, is in a tetrahedral coordination environment and the environment of each N atom is essentially planar (sums of angles = 359.7, 359.9and 358.4°). The phosphoryl and carbonyl groups adopt anti orientations with respect to each other. In the crystal, adjacent molecules are linked via N-H···O=P and two N-H···O=C hydrogen bonds into an extended chain parallel to the *a* axis.

Related literature

For a phosphorus ligand having a C(O)NHP(O) skeleton, see: Gholivand et al. (2010). For a related structure, see: Pourayoubi et al. (2010). For bond lengths in related structures, see: Sabbaghi et al. (2010) and references cited therein.



Experimental

Crystal data

C21H21FN3O2P V = 2007.5 (3) Å³ $M_r = 397.38$ Z = 4Monoclinic, $P2_1/n$ a = 9.7697 (9) Å $\mu = 0.17 \text{ mm}^$ b = 10.2197 (9) Å T = 100 Kc = 20.2404 (18) Å $\beta = 96.605 (1)^{\circ}$

Data collection

Bruker SMART CCD area-detector diffractometer Absorption correction: multi-scan (SADABS; Bruker, 2005) $T_{\rm min} = 0.959, \ T_{\rm max} = 0.975$

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.046$	
$vR(F^2) = 0.127$	
S = 1.05	
1551 reflections	
264 parameters	
3 restraints	

Mo $K\alpha$ radiation $0.25 \times 0.15 \times 0.15 \mbox{ mm}$

15865 measured reflections 4551 independent reflections 3411 reflections with $I > 2\sigma(I)$ $R_{\rm int} = 0.035$

H atoms treated by a mixture of independent and constrained refinement $\Delta \rho_{\text{max}} = 0.41 \text{ e } \text{\AA}^{-3}$ $\Delta \rho_{\rm min} = -0.26 \text{ e } \text{\AA}^{-3}$

Table 1 Hydrogen-bond geometry (Å, °).

$D - H \cdots A$	D-H	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdots A$
$N1 - H1N \cdots O2^{i}$ $N2 - H2N \cdots O1^{ii}$ $N3 - H3N \cdots O1^{ii}$	$\begin{array}{c} 0.87 \ (1) \\ 0.86 \ (1) \\ 0.86 \ (1) \end{array}$	1.92 (1) 2.08 (1) 2.24 (2)	2.780 (2) 2.886 (2) 2.945 (2)	171 (2) 156 (2) 139 (2)

Symmetry codes: (i) -x + 1, -y + 2, -z + 1; (ii) -x + 2, -y + 2, -z + 1.

Data collection: SMART (Bruker, 2005); cell refinement: SAINT (Bruker, 2005); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: SHELXTL (Sheldrick, 2008); software used to prepare material for publication: SHELXTL and enCIFer (Allen et al., 2004).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: NC2222).

References

- Allen, F. H., Johnson, O., Shields, G. P., Smith, B. R. & Towler, M. (2004). J. Appl. Cryst. 37, 335-338.
- Bruker (2005). SADABS, SMART and SAINT. Bruker AXS Inc., Madison, Wisconsin, USA.
- Gholivand, K., Mahzouni, H. R., Pourayoubi, M. & Amiri, S. (2010). Inorg. Chim. Acta. 363, 2318-2324.
- Pourayoubi, M., Tarahhomi, A., Rheingold, A. L. & Golen, J. A. (2010). Acta Crvst. E66, 02524.
- Sabbaghi, F., Pourayoubi, M., Toghraee, M. & Divjakovic, V. (2010). Acta Cryst. E66, 0344.
- Sheldrick, G. M. (2008). Acta Cryst. A64, 112-122.

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N-(2-Fluorobenzoyl)-*N*',*N*''-bis(4-methylphenyl)phosphoric triamide

M. Pourayoubi, A. Tarahhomi, A. L. Rheingold and J. A. Golen

Comment

Carbacylamidophosphates with a C(O)NHP(O) skeleton have attracted attention because of their roles as the O,O'-donor ligands for metal complexation (Gholivand *et al.*, 2010). Following the previous works about carbacylamidophosphates such as P(O)[NHC(O)C₆H₃(2,6-F₂)][N(CH₃)(CH₂C₆H₅)]₂ (Pourayoubi *et al.*, 2010), here, we report on the synthesis and crystal structure of the title compound, P(O)[NHC(O)C₆H₄(2-F)][NH—C₆H₄-4-CH₃]₂.

In the crystal structure of the title compound the phosphoryl and carbonyl groups adopt *anti* positions to each other. The P atom has a slightly distorted tetrahedral configuration (Fig. 1). The bond angles around the P atom are in the range of 101.09 (8)° to 116.67 (8)°. The P1—N2 and P1—N3 bonds (1.6361 (15) Å and 1.6291 (17) Å) are shorter than the P1—N1 bond (1.6872 (15) Å). The environment of the nitrogen atoms is essentially planar. The P=O bond length of 1.4723 (13) Å is comparable to those in similar compounds *e.g.* in P(O)[NHC(O)C₆H₄(4-NO₂)][NHC₆H₁₁]₂ (Sabbaghi *et al.*, 2010).

In the crystal structure, adjacent molecules are linked *via* $N_{C(O)NHP(O)}$ —H···O =P and two N_{amide} —H···O =C hydrogen bonds (see Table 1), into an extended chain parallel to the *a* axis.

Experimental

 $2-F-C_6H_4C(O)NHP(O)Cl_2$ has been synthesized from the reaction between phosphorus pentachloride (4.0 g, 19.2 mmol) and 2-fluorobenzamide (2.671 g, 19.2 mmol) in dry CCl₄ at 358 K (3 h) and then the treatment of formic acid (0.884 g, 19.2 mmol) at ice bath temperature. To a solution of $2-F-C_6H_4C(O)NHP(O)Cl_2$ (0.3 g, 1.17 mmol) in dry chloroform (30 ml), a mixture of *p*-toluidine (0.251 g, 2.34 mmol) and triethylamine (0.237 g, 2.34 mmol) in dry chloroform (10 ml) was added at 273 k. After 4 h stirring, the solvent was removed and the product was washed with distilled water and recrystallized from methanol/chloroform at room temperature. IR (KBr, cm⁻¹): 3308 (NH), 3030 (NH), 2896, 2627, 1639 (C=O), 1457, 1220, 1061, 944, 795.

Refinement

Hydrogen atoms H1N, H2N, and H3N were located in Fourier difference map and were refined with DFIX 0.88 (0.01) for the N–H bond lengths and isotropic displacement parameter of 1.2 times U_{eq} of the parent N atoms. All other hydrogen atoms were placed in their calculated positions with atom–H lengths of 0.95 Å (CH) and 0.98 Å (CH3) and isotropic displacement parameters for these atoms were set to 1.20 times (CH) and 1.50 times (CH₃) U_{eq} of the parent C atom.

Figures



Fig. 1. An *ORTEP*-style plot of title compound with labeling. Displacement ellipsoids are drawn at the 50% probability level.

N-{bis[(4-methylphenyl)amino]phosphoryl}-2-fluorobenzamide

Crystal data	
$C_{21}H_{21}FN_3O_2P$	F(000) = 832
$M_r = 397.38$	$D_{\rm x} = 1.315 {\rm ~Mg~m}^{-3}$
Monoclinic, $P2_1/n$	Mo <i>K</i> α radiation, $\lambda = 0.71073$ Å
a = 9.7697 (9) Å	Cell parameters from 5744 reflections
b = 10.2197 (9) Å	$\theta = 2.2 - 27.5^{\circ}$
c = 20.2404 (18) Å	$\mu = 0.17 \text{ mm}^{-1}$
$\beta = 96.605 \ (1)^{\circ}$	T = 100 K
V = 2007.5 (3) Å ³	Block, colourless
Z = 4	$0.25\times0.15\times0.15~mm$

Data collection

Bruker SMART CCD area-detector diffractometer	4551 independent reflections
Radiation source: fine-focus sealed tube	3411 reflections with $I > 2\sigma(I)$
graphite	$R_{\rm int} = 0.035$
ϕ and ω scans	$\theta_{\text{max}} = 27.9^{\circ}, \ \theta_{\text{min}} = 2.0^{\circ}$
Absorption correction: multi-scan (<i>SADABS</i> ; Bruker, 2005)	$h = -12 \rightarrow 12$
$T_{\min} = 0.959, T_{\max} = 0.975$	$k = -11 \rightarrow 13$
15865 measured reflections	$l = -25 \rightarrow 25$

Refinement

Refinement on F^2	Primary atom site location: structure-invariant direct methods
Least-squares matrix: full	Secondary atom site location: difference Fourier map
$R[F^2 > 2\sigma(F^2)] = 0.046$	Hydrogen site location: inferred from neighbouring sites
$wR(F^2) = 0.127$	H atoms treated by a mixture of independent and constrained refinement
<i>S</i> = 1.05	$w = 1/[\sigma^2(F_o^2) + (0.0669P)^2 + 0.498P]$ where $P = (F_o^2 + 2F_c^2)/3$
4551 reflections	$(\Delta/\sigma)_{\rm max} = 0.007$

264 parameters	$\Delta \rho_{max} = 0.41 \text{ e} \text{ Å}^{-3}$
3 restraints	$\Delta \rho_{\rm min} = -0.26 \text{ e } \text{\AA}^{-3}$

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

	x	у	Ζ	$U_{\rm iso}*/U_{\rm eq}$
P1	0.72255 (5)	0.92119 (4)	0.50855 (2)	0.02136 (14)
F1	0.92737 (14)	1.40039 (12)	0.55287 (6)	0.0441 (3)
01	0.91560 (13)	1.14443 (13)	0.50431 (6)	0.0293 (3)
02	0.58757 (12)	0.86140 (12)	0.51487 (6)	0.0250 (3)
N1	0.69300 (16)	1.08365 (14)	0.50258 (7)	0.0210 (3)
H1N	0.6074 (11)	1.1095 (19)	0.4983 (9)	0.025*
N2	0.79772 (16)	0.87866 (15)	0.44363 (8)	0.0240 (3)
H2N	0.8811 (12)	0.8507 (19)	0.4525 (10)	0.029*
N3	0.84260 (16)	0.88686 (16)	0.56874 (8)	0.0267 (4)
H3N	0.9270 (12)	0.905 (2)	0.5636 (10)	0.032*
C1	0.8139 (2)	1.41838 (19)	0.50898 (9)	0.0296 (4)
C2	0.7701 (2)	1.5451 (2)	0.49516 (11)	0.0381 (5)
H2C	0.8194	1.6173	0.5157	0.046*
C3	0.6533 (2)	1.5647 (2)	0.45090 (11)	0.0379 (5)
H3B	0.6219	1.6511	0.4408	0.045*
C4	0.5822 (2)	1.4596 (2)	0.42132 (11)	0.0344 (5)
H4A	0.5029	1.4737	0.3903	0.041*
C5	0.6265 (2)	1.33331 (19)	0.43680 (9)	0.0278 (4)
H5A	0.5765	1.2612	0.4166	0.033*
C6	0.74372 (19)	1.31052 (17)	0.48164 (9)	0.0230 (4)
C7	0.79305 (18)	1.17460 (18)	0.49728 (8)	0.0220 (4)
C8	0.7441 (2)	0.89104 (17)	0.37612 (9)	0.0244 (4)
С9	0.6203 (2)	0.9545 (2)	0.35614 (10)	0.0319 (5)
H9A	0.5685	0.9914	0.3884	0.038*
C10	0.5725 (2)	0.9640 (2)	0.28921 (10)	0.0360 (5)
H10A	0.4886	1.0089	0.2762	0.043*
C11	0.6439 (2)	0.9096 (2)	0.24070 (10)	0.0404 (5)
C12	0.7657 (2)	0.8443 (2)	0.26118 (10)	0.0419 (6)
H12A	0.8157	0.8051	0.2288	0.050*
C13	0.8164 (2)	0.8347 (2)	0.32801 (10)	0.0341 (5)

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (A^2)

H13A	0.9004	0.7898	0.3409	0.041*
C14	0.5884 (3)	0.9202 (3)	0.16774 (11)	0.0561 (7)
H14A	0.6098	0.8398	0.1446	0.084*
H14B	0.6313	0.9950	0.1479	0.084*
H14C	0.4884	0.9326	0.1636	0.084*
C15	0.8269 (2)	0.85706 (18)	0.63606 (9)	0.0260 (4)
C16	0.7217 (2)	0.7756 (2)	0.65213 (10)	0.0406 (5)
H16A	0.6570	0.7408	0.6180	0.049*
C17	0.7115 (2)	0.7452 (3)	0.71817 (11)	0.0506 (7)
H17A	0.6367	0.6929	0.7288	0.061*
C18	0.8072 (3)	0.7891 (2)	0.76906 (10)	0.0435 (6)
C19	0.9162 (3)	0.8633 (2)	0.75138 (11)	0.0507 (7)
H19A	0.9862	0.8909	0.7850	0.061*
C20	0.9253 (3)	0.8980 (2)	0.68584 (11)	0.0427 (6)
H20A	1.0000	0.9504	0.6752	0.051*
C21	0.7964 (3)	0.7510(3)	0.84055 (11)	0.0657 (8)
H21A	0.8791	0.7801	0.8687	0.099*
H21B	0.7879	0.6557	0.8437	0.099*
H21C	0.7150	0.7926	0.8556	0.099*

Atomic displacement parameters (\AA^2)

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
P1	0.0143 (3)	0.0263 (2)	0.0236 (2)	0.00103 (18)	0.00229 (18)	0.00314 (18)
F1	0.0442 (8)	0.0440 (7)	0.0404 (7)	-0.0137 (6)	-0.0116 (6)	-0.0023 (5)
01	0.0150 (7)	0.0379 (8)	0.0351 (8)	-0.0004 (6)	0.0030 (6)	0.0005 (6)
02	0.0142 (7)	0.0278 (7)	0.0330 (7)	-0.0001 (5)	0.0025 (5)	0.0038 (5)
N1	0.0143 (8)	0.0244 (8)	0.0245 (8)	0.0002 (6)	0.0038 (6)	0.0007 (6)
N2	0.0158 (8)	0.0297 (8)	0.0262 (8)	0.0048 (6)	0.0015 (6)	-0.0003 (6)
N3	0.0133 (8)	0.0388 (9)	0.0279 (9)	0.0000 (7)	0.0018 (7)	0.0086 (6)
C1	0.0288 (11)	0.0346 (11)	0.0252 (10)	-0.0079 (9)	0.0024 (8)	-0.0004 (8)
C2	0.0497 (15)	0.0292 (10)	0.0368 (12)	-0.0104 (10)	0.0106 (10)	-0.0051 (9)
C3	0.0433 (14)	0.0280 (11)	0.0443 (12)	0.0005 (9)	0.0135 (11)	0.0062 (9)
C4	0.0271 (11)	0.0353 (11)	0.0411 (12)	0.0002 (9)	0.0058 (9)	0.0084 (9)
C5	0.0231 (10)	0.0292 (10)	0.0317 (10)	-0.0033 (8)	0.0057 (8)	0.0011 (8)
C6	0.0202 (10)	0.0273 (9)	0.0227 (9)	-0.0035 (7)	0.0073 (7)	-0.0015 (7)
C7	0.0167 (10)	0.0303 (9)	0.0192 (9)	-0.0013 (7)	0.0033 (7)	-0.0019 (7)
C8	0.0212 (10)	0.0274 (9)	0.0247 (9)	-0.0034 (8)	0.0032 (8)	0.0010 (7)
С9	0.0270 (11)	0.0404 (11)	0.0278 (10)	0.0020 (9)	0.0019 (8)	-0.0030 (8)
C10	0.0290 (12)	0.0461 (12)	0.0313 (11)	0.0001 (10)	-0.0038 (9)	0.0029 (9)
C11	0.0345 (13)	0.0601 (15)	0.0262 (11)	-0.0110 (11)	0.0015 (9)	0.0024 (9)
C12	0.0351 (13)	0.0624 (15)	0.0300 (12)	-0.0047 (11)	0.0109 (10)	-0.0062 (10)
C13	0.0254 (11)	0.0452 (12)	0.0324 (11)	0.0013 (9)	0.0060 (9)	-0.0017 (9)
C14	0.0465 (16)	0.095 (2)	0.0262 (12)	-0.0108 (14)	0.0008 (11)	0.0069 (12)
C15	0.0234 (10)	0.0299 (10)	0.0248 (10)	0.0057 (8)	0.0040 (8)	0.0025 (7)
C16	0.0266 (12)	0.0627 (15)	0.0318 (11)	-0.0063 (10)	0.0001 (9)	0.0129 (10)
C17	0.0322 (13)	0.0782 (18)	0.0421 (14)	-0.0019 (12)	0.0075 (11)	0.0229 (12)
C18	0.0496 (15)	0.0558 (14)	0.0263 (11)	0.0136 (12)	0.0098 (10)	0.0039 (9)

C19	0.0709 (19)	0.0504 (14)	0.0284 (12)	-0.0100 (13)	-0.0048 (12)	-0.0038 (10)
C20	0.0499 (15)	0.0433 (13)	0.0336 (12)	-0.0166 (11)	-0.0006 (10)	0.0005 (9)
C21	0.074 (2)	0.095 (2)	0.0310 (13)	0.0190 (17)	0.0163 (13)	0.0111 (13)
Geometric param	neters (Å, °)					
P1—O2		1.4723 (13)	C9—I	H9A	0.95	00
P1—N3		1.6291 (17)	C10—	-C11	1.38	5 (3)
P1—N2		1.6361 (15)	C10—	-H10A	0.95	00
P1—N1		1.6872 (15)	C11—	-C12	1.38	6 (3)
F1—C1		1.351 (2)	C11—	-C14	1.51	7 (3)
O1—C7		1.229 (2)	C12—	-C13	1.38	9 (3)
N1—C7		1.362 (2)	C12—	-H12A	0.95	00
N1—H1N		0.872 (9)	C13—	-H13A	0.95	00
N2—C8		1.412 (2)	C14—	-H14A	0.98	00
N2—H2N		0.862 (9)	C14—	-H14B	0.98	00
N3—C15		1.422 (2)	C14—	-H14C	0.98	00
N3—H3N		0.863 (9)	C15—	-C20	1.37	5 (3)
C1—C6		1.380 (3)	C15—	-C16	1.39	0 (3)
C1—C2		1.382 (3)	C16—	-C17	1.38	7 (3)
C2—C3		1.382 (3)	C16—	-H16A	0.95	00
C2—H2C		0.9500	C17—	-C18	1.38	4 (3)
C3—C4		1.378 (3)	C17—	-H17A	0.95	00
C3—H3B		0.9500	C18—	-C19	1.38	7 (3)
C4—C5		1.385 (3)	C18—	-C21	1.51	4 (3)
C4—H4A		0.9500	C19—	-C20	1.38	6 (3)
C5—C6		1.396 (3)	C19—	-H19A	0.95	00
C5—H5A		0.9500	C20—	-H20A	0.95	00
C6—C7		1.492 (3)	C21—	-H21A	0.98	00
C8—C9		1.391 (3)	C21—	-H21B	0.98	00
C8—C13		1.392 (3)	C21—	-H21C	0.98	00
C9—C10		1.384 (3)				
O2—P1—N3		114.88 (8)	С9—(C10—C11	121.	7 (2)
O2—P1—N2		116.67 (8)	С9—(C10—H10A	119.	2
N3—P1—N2		101.09 (8)	C11—	-C10—H10A	119.	2
O2—P1—N1		105.49 (8)	C10-	-C11C12	117.	8 (2)
N3—P1—N1		111.59 (8)	C10-	-C11C14	120.	6 (2)
N2—P1—N1		107.03 (8)	C12—	-C11C14	121.	6 (2)
C7—N1—P1		123.97 (13)	C11-	-C12C13	121.	5 (2)
C7—N1—H1N		118.3 (13)	C11-	-C12—H12A	119.	2
P1—N1—H1N		117.4 (13)	C13—	-C12—H12A	119.	2
C8—N2—P1		127.06 (13)	C12—	-C13—C8	120.	0 (2)
C8—N2—H2N		117.9 (13)	C12—	-C13—H13A	120.	0
P1—N2—H2N		114.9 (13)	C8—0	C13—H13A	120.	0
C15—N3—P1		127.97 (13)	C11-	-C14—H14A	109.	5
C15—N3—H3N		111.7 (14)	C11-	-C14—H14B	109.	5
P1 - N3 - H3N		118.7 (14)	H14A	—C14—H14B	109.	5
F1—C1—C6		119.15 (18)	C11-	-C14—H14C	109.	5
F1-C1-C2		118.14 (18)	H14A	—C14—H14C	109.	5

C6—C1—C2	122.7 (2)	H14B—C14—H14C	109.5
C3—C2—C1	118.7 (2)	C20—C15—C16	118.94 (18)
C3—C2—H2C	120.7	C20—C15—N3	119.60 (18)
C1—C2—H2C	120.7	C16—C15—N3	121.11 (18)
C4—C3—C2	120.4 (2)	C17—C16—C15	119.8 (2)
С4—С3—Н3В	119.8	С17—С16—Н16А	120.1
С2—С3—Н3В	119.8	C15—C16—H16A	120.1
C3—C4—C5	119.9 (2)	C18—C17—C16	121.8 (2)
C3—C4—H4A	120.0	C18—C17—H17A	119.1
C5—C4—H4A	120.0	С16—С17—Н17А	119.1
C4—C5—C6	120.93 (19)	C17—C18—C19	117.3 (2)
С4—С5—Н5А	119.5	C17—C18—C21	120.8 (2)
С6—С5—Н5А	119.5	C19—C18—C21	121.8 (2)
C1—C6—C5	117.37 (18)	C20-C19-C18	121.5 (2)
C1—C6—C7	121.68 (18)	С20—С19—Н19А	119.2
C5—C6—C7	120.92 (16)	C18—C19—H19A	119.2
O1—C7—N1	121.22 (17)	C15—C20—C19	120.5 (2)
O1—C7—C6	123.01 (16)	C15—C20—H20A	119.8
N1—C7—C6	115.77 (15)	С19—С20—Н20А	119.8
C9—C8—C13	118.93 (18)	C18—C21—H21A	109.5
C9—C8—N2	122.47 (16)	C18—C21—H21B	109.5
C13—C8—N2	118.58 (17)	H21A—C21—H21B	109.5
C10—C9—C8	120.08 (18)	C18—C21—H21C	109.5
С10—С9—Н9А	120.0	H21A—C21—H21C	109.5
С8—С9—Н9А	120.0	H21B—C21—H21C	109.5
Ω_{2} P1 N1 C7	178 66 (14)	C5-C6-C7-N1	-390(2)
	1/0.00 (11)	CJ-C0-C/-N1	57.0(2)
N3—P1—N1—C7	53.27 (16)	P1—N2—C8—C9	6.1 (3)
N3—P1—N1—C7 N2—P1—N1—C7	53.27 (16) -56.46 (16)	P1—N2—C8—C9 P1—N2—C8—C13	6.1 (3) -172.26 (15)
N3—P1—N1—C7 N2—P1—N1—C7 O2—P1—N2—C8	53.27 (16) -56.46 (16) 57.27 (18)	P1—N2—C8—C9 P1—N2—C8—C13 C13—C8—C9—C10	6.1 (3) -172.26 (15) -1.7 (3)
N3—P1—N1—C7 N2—P1—N1—C7 O2—P1—N2—C8 N3—P1—N2—C8	53.27 (16) -56.46 (16) 57.27 (18) -177.42 (15)	P1—N2—C8—C9 P1—N2—C8—C13 C13—C8—C9—C10 N2—C8—C9—C10	6.1 (3) -172.26 (15) -1.7 (3) 179.93 (18)
N3—P1—N1—C7 N2—P1—N1—C7 O2—P1—N2—C8 N3—P1—N2—C8 N1—P1—N2—C8	53.27 (16) -56.46 (16) 57.27 (18) -177.42 (15) -60.53 (17)	P1—N2—C8—C9 P1—N2—C8—C13 C13—C8—C9—C10 N2—C8—C9—C10 C8—C9—C10—C11	6.1 (3) -172.26 (15) -1.7 (3) 179.93 (18) 1.1 (3)
N3—P1—N1—C7 N2—P1—N1—C7 O2—P1—N2—C8 N3—P1—N2—C8 N1—P1—N2—C8 O2—P1—N3—C15	53.27 (16) -56.46 (16) 57.27 (18) -177.42 (15) -60.53 (17) -28.7 (2)	P1—N2—C8—C9 P1—N2—C8—C13 C13—C8—C9—C10 N2—C8—C9—C10 C8—C9—C10—C11 C9—C10—C11—C12	6.1 (3) -172.26 (15) -1.7 (3) 179.93 (18) 1.1 (3) 0.3 (3)
N3—P1—N1—C7 N2—P1—N1—C7 O2—P1—N2—C8 N3—P1—N2—C8 N1—P1—N2—C8 O2—P1—N3—C15 N2—P1—N3—C15	53.27 (16) -56.46 (16) 57.27 (18) -177.42 (15) -60.53 (17) -28.7 (2) -155.21 (16)	P1—N2—C8—C9 P1—N2—C8—C13 C13—C8—C9—C10 N2—C8—C9—C10 C8—C9—C10—C11 C9—C10—C11—C12 C9—C10—C11—C14	6.1 (3) -172.26 (15) -1.7 (3) 179.93 (18) 1.1 (3) 0.3 (3) 179.3 (2)
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$	53.27 (16) -56.46 (16) 57.27 (18) -177.42 (15) -60.53 (17) -28.7 (2) -155.21 (16) 91.30 (17)	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$	6.1 (3) -172.26 (15) -1.7 (3) 179.93 (18) 1.1 (3) 0.3 (3) 179.3 (2) -0.9 (3)
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$	53.27 (16) $-56.46 (16)$ $57.27 (18)$ $-177.42 (15)$ $-60.53 (17)$ $-28.7 (2)$ $-155.21 (16)$ $91.30 (17)$ $-179.31 (17)$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$	6.1 (3) -172.26 (15) -1.7 (3) 179.93 (18) 1.1 (3) 0.3 (3) 179.3 (2) -0.9 (3) 180.0 (2)
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$ $C6 - C1 - C2 - C3$	53.27 (16) -56.46 (16) 57.27 (18) -177.42 (15) -60.53 (17) -28.7 (2) -155.21 (16) 91.30 (17) -179.31 (17) -1.7 (3)	P1—N2—C8—C9 P1—N2—C8—C9 P1—N2—C8—C13 C13—C8—C9—C10 N2—C8—C9—C10 C8—C9—C10—C11 C9—C10—C11—C12 C9—C10—C11—C12 C10—C11—C12—C13 C14—C11—C12—C13 C11—C12—C13—C8	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \end{array}$
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$ $C6 - C1 - C2 - C3$ $C1 - C2 - C3 - C4$	53.27 (16) $-56.46 (16)$ $57.27 (18)$ $-177.42 (15)$ $-60.53 (17)$ $-28.7 (2)$ $-155.21 (16)$ $91.30 (17)$ $-179.31 (17)$ $-1.7 (3)$ $0.1 (3)$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \end{array}$
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$ $C6 - C1 - C2 - C3$ $C1 - C2 - C3 - C4$ $C2 - C3 - C4 - C5$	53.27 (16) $-56.46 (16)$ $57.27 (18)$ $-177.42 (15)$ $-60.53 (17)$ $-28.7 (2)$ $-155.21 (16)$ $91.30 (17)$ $-179.31 (17)$ $-1.7 (3)$ $0.1 (3)$ $1.1 (3)$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $N2-C8-C13-C12$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \end{array}$
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$ $C6 - C1 - C2 - C3$ $C1 - C2 - C3 - C4$ $C2 - C3 - C4 - C5$ $C3 - C4 - C5 - C6$	53.27 (16) $-56.46 (16)$ $57.27 (18)$ $-177.42 (15)$ $-60.53 (17)$ $-28.7 (2)$ $-155.21 (16)$ $91.30 (17)$ $-179.31 (17)$ $-1.7 (3)$ $0.1 (3)$ $1.1 (3)$ $-0.7 (3)$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $N2-C8-C13-C12$ $P1-N3-C15-C20$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \end{array}$
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$ $C6 - C1 - C2 - C3$ $C1 - C2 - C3 - C4$ $C2 - C3 - C4 - C5$ $C3 - C4 - C5 - C6$ $F1 - C1 - C6 - C5$	53.27 (16) $-56.46 (16)$ $57.27 (18)$ $-177.42 (15)$ $-60.53 (17)$ $-28.7 (2)$ $-155.21 (16)$ $91.30 (17)$ $-179.31 (17)$ $-1.7 (3)$ $0.1 (3)$ $1.1 (3)$ $-0.7 (3)$ $179.64 (15)$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $N2-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \end{array}$
$N_{3} = P_{1} = N_{1} = C_{7}$ $N_{2} = P_{1} = N_{1} = C_{7}$ $O_{2} = P_{1} = N_{2} = C_{8}$ $N_{3} = P_{1} = N_{2} = C_{8}$ $O_{2} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{1} = P_{1} = N_{3} = C_{15}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{5}$ $C_{2} = C_{1} = C_{6} = C_{5}$	53.27 (16) $-56.46 (16)$ $57.27 (18)$ $-177.42 (15)$ $-60.53 (17)$ $-28.7 (2)$ $-155.21 (16)$ $91.30 (17)$ $-179.31 (17)$ $-1.7 (3)$ $0.1 (3)$ $1.1 (3)$ $-0.7 (3)$ $179.64 (15)$ $2.0 (3)$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $N2-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 4.9 (3) \end{array}$
$N_{3} = P_{1} = N_{1} = C_{7}$ $N_{2} = P_{1} = N_{1} = C_{7}$ $O_{2} = P_{1} = N_{2} = C_{8}$ $N_{3} = P_{1} = N_{2} = C_{8}$ $O_{2} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{1} = P_{1} = N_{3} = C_{15}$ $C_{2} = C_{1} = C_{3} = C_{4}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5}$ $C_{2} = C_{1} = C_{6} = C_{5}$ $F_{1} = C_{1} = C_{6} = C_{7}$	$\begin{array}{c} 1.10.00 \ (11) \\ 53.27 \ (16) \\ -56.46 \ (16) \\ 57.27 \ (18) \\ -177.42 \ (15) \\ -60.53 \ (17) \\ -28.7 \ (2) \\ -155.21 \ (16) \\ 91.30 \ (17) \\ -179.31 \ (17) \\ -1.7 \ (3) \\ 0.1 \ (3) \\ 1.1 \ (3) \\ -0.7 \ (3) \\ 179.64 \ (15) \\ 2.0 \ (3) \\ -2.4 \ (3) \end{array}$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $N2-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$ $N3-C15-C16-C17$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 4.9 (3) \\ 178.1 (2) \end{array}$
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$ $C6 - C1 - C2 - C3$ $C1 - C2 - C3 - C4$ $C2 - C3 - C4 - C5$ $C3 - C4 - C5 - C6$ $F1 - C1 - C6 - C5$ $F1 - C1 - C6 - C5$ $F1 - C1 - C6 - C7$ $C2 - C1 - C6 - C7$	53.27 (16) $-56.46 (16)$ $57.27 (18)$ $-177.42 (15)$ $-60.53 (17)$ $-28.7 (2)$ $-155.21 (16)$ $91.30 (17)$ $-179.31 (17)$ $-1.7 (3)$ $0.1 (3)$ $1.1 (3)$ $-0.7 (3)$ $179.64 (15)$ $2.0 (3)$ $-2.4 (3)$ $179.95 (17)$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$ $N3-C15-C16-C17$ $C15-C16-C17$ $C15-C16-C17-C18$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 4.9 (3) \\ 178.1 (2) \\ -3.0 (4) \end{array}$
$N_{3} = P_{1} = N_{1} = C_{7}$ $N_{2} = P_{1} = N_{1} = C_{7}$ $O_{2} = P_{1} = N_{2} = C_{8}$ $N_{3} = P_{1} = N_{2} = C_{8}$ $O_{2} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{1} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1} = C_{1} = C_{15}$ $N_{1} = C_{1} = C_{1}$	$\begin{array}{c} 1.10.00 \ (11) \\ 53.27 \ (16) \\ -56.46 \ (16) \\ 57.27 \ (18) \\ -177.42 \ (15) \\ -60.53 \ (17) \\ -28.7 \ (2) \\ -155.21 \ (16) \\ 91.30 \ (17) \\ -179.31 \ (17) \\ -1.7 \ (3) \\ 0.1 \ (3) \\ 1.1 \ (3) \\ -0.7 \ (3) \\ 179.64 \ (15) \\ 2.0 \ (3) \\ -2.4 \ (3) \\ 179.95 \ (17) \\ -0.8 \ (3) \end{array}$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$ $N3-C15-C16-C17$ $N3-C15-C16-C17$ $C15-C16-C17-C18$ $C16-C17-C18$ $C16-C17-C18-C19$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 4.9 (3) \\ 178.1 (2) \\ -3.0 (4) \\ -1.2 (4) \end{array}$
$N_{3} = P_{1} = N_{1} = C_{7}$ $N_{2} = P_{1} = N_{1} = C_{7}$ $O_{2} = P_{1} = N_{2} = C_{8}$ $N_{3} = P_{1} = N_{2} = C_{8}$ $O_{2} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{1} = P_{1} = N_{3} = C_{15}$ $N_{1} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $C_{4} = C_{5} = C_{6} = C_{1}$ $C_{4} = C_{5} = C_{6} = C_{7}$	$\begin{array}{c} 1.10.00 \ (11) \\ 53.27 \ (16) \\ -56.46 \ (16) \\ 57.27 \ (18) \\ -177.42 \ (15) \\ -60.53 \ (17) \\ -28.7 \ (2) \\ -155.21 \ (16) \\ 91.30 \ (17) \\ -179.31 \ (17) \\ -1.7 \ (3) \\ 0.1 \ (3) \\ 1.1 \ (3) \\ -0.7 \ (3) \\ 179.64 \ (15) \\ 2.0 \ (3) \\ -2.4 \ (3) \\ 179.95 \ (17) \\ -0.8 \ (3) \\ -178.77 \ (17) \end{array}$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $N2-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$ $N3-C15-C16-C17$ $C15-C16-C17-C18$ $C16-C17-C18-C19$ $C16-C17-C18-C21$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 4.9 (3) \\ 178.1 (2) \\ -3.0 (4) \\ -1.2 (4) \\ -178.0 (2) \end{array}$
$N_{3} = P_{1} = N_{1} = C_{7}$ $N_{2} = P_{1} = N_{1} = C_{7}$ $O_{2} = P_{1} = N_{2} = C_{8}$ $N_{3} = P_{1} = N_{2} = C_{8}$ $O_{2} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{1} = P_{1} = N_{3} = C_{15}$ $C_{2} = C_{1} = C_{2} = C_{3}$ $C_{4} = C_{5} = C_{6}$ $F_{1} = C_{1} = C_{6} = C_{7}$ $C_{4} = C_{5} = C_{6} = C_{7}$ $P_{1} = N_{1} = C_{7} = O_{1}$	$\begin{array}{c} 170.00 \ (11) \\ 53.27 \ (16) \\ -56.46 \ (16) \\ 57.27 \ (18) \\ -177.42 \ (15) \\ -60.53 \ (17) \\ -28.7 \ (2) \\ -155.21 \ (16) \\ 91.30 \ (17) \\ -155.21 \ (16) \\ 91.30 \ (17) \\ -179.31 \ (17) \\ -1.7 \ (3) \\ 0.1 \ (3) \\ 1.1 \ (3) \\ -0.7 \ (3) \\ 179.64 \ (15) \\ 2.0 \ (3) \\ -2.4 \ (3) \\ 179.95 \ (17) \\ -0.8 \ (3) \\ -178.77 \ (17) \\ -8.6 \ (2) \end{array}$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$ $N3-C15-C16-C17$ $C15-C16-C17-C18$ $C16-C17-C18-C19$ $C16-C17-C18-C21$ $C17-C18-C19-C20$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 4.9 (3) \\ 178.1 (2) \\ -3.0 (4) \\ -1.2 (4) \\ -178.0 (2) \\ 3.3 (4) \end{array}$
N3 - P1 - N1 - C7 $N2 - P1 - N1 - C7$ $O2 - P1 - N2 - C8$ $N3 - P1 - N2 - C8$ $O2 - P1 - N3 - C15$ $N2 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $N1 - P1 - N3 - C15$ $F1 - C1 - C2 - C3$ $C6 - C1 - C2 - C3$ $C1 - C2 - C3 - C4$ $C2 - C3 - C4 - C5$ $C3 - C4 - C5 - C6$ $F1 - C1 - C6 - C5$ $F1 - C1 - C6 - C7$ $C2 - C1 - C6 - C7$ $C4 - C5 - C6 - C1$ $P1 - N1 - C7 - O1$ $P1 - N1 - C7 - C6$	$\begin{array}{c} 170.00 \ (11) \\ 53.27 \ (16) \\ -56.46 \ (16) \\ 57.27 \ (18) \\ -177.42 \ (15) \\ -60.53 \ (17) \\ -28.7 \ (2) \\ -155.21 \ (16) \\ 91.30 \ (17) \\ -179.31 \ (17) \\ -179.31 \ (17) \\ -1.7 \ (3) \\ 0.1 \ (3) \\ 1.1 \ (3) \\ -0.7 \ (3) \\ 179.64 \ (15) \\ 2.0 \ (3) \\ -2.4 \ (3) \\ 179.95 \ (17) \\ -0.8 \ (3) \\ -178.77 \ (17) \\ -8.6 \ (2) \\ 170.55 \ (12) \end{array}$	P1-N2-C8-C9 $P1-N2-C8-C9$ $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$ $N3-C15-C16-C17$ $N3-C15-C16-C17$ $N3-C15-C16-C17$ $C15-C16-C17-C18$ $C16-C17-C18-C19$ $C16-C17-C18-C21$ $C17-C18-C19-C20$ $C21-C18-C19-C20$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 4.9 (3) \\ 178.1 (2) \\ -3.0 (4) \\ -1.2 (4) \\ -178.0 (2) \\ 3.3 (4) \\ -179.9 (2) \end{array}$
$N_{3} = P_{1} = N_{1} = C_{7}$ $N_{2} = P_{1} = N_{1} = C_{7}$ $O_{2} = P_{1} = N_{2} = C_{8}$ $N_{3} = P_{1} = N_{2} = C_{8}$ $O_{2} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $N_{1} = P_{1} = N_{3} = C_{15}$ $N_{2} = P_{1} = N_{3} = C_{15}$ $C_{2} = C_{1} = C_{2} = C_{3}$ $C_{4} = C_{5} = C_{6}$ C_{7} $C_{4} = C_{5} = C_{6} = C_{7}$ $P_{1} = N_{1} = C_{7} = C_{6}$ $C_{1} = C_{6} = C_{7} = C_{1}$ $P_{1} = N_{1} = C_{7} = C_{6}$	$\begin{array}{c} 1.10.00 \ (11) \\ 53.27 \ (16) \\ -56.46 \ (16) \\ 57.27 \ (18) \\ -177.42 \ (15) \\ -60.53 \ (17) \\ -28.7 \ (2) \\ -155.21 \ (16) \\ 91.30 \ (17) \\ -179.31 \ (17) \\ -1.7 \ (3) \\ 0.1 \ (3) \\ 1.1 \ (3) \\ -0.7 \ (3) \\ 179.64 \ (15) \\ 2.0 \ (3) \\ -2.4 \ (3) \\ 179.95 \ (17) \\ -0.8 \ (3) \\ -178.77 \ (17) \\ -8.6 \ (2) \\ 170.55 \ (12) \\ -37.7 \ (3) \end{array}$	P1-N2-C8-C9 $P1-N2-C8-C13$ $C13-C8-C9-C10$ $N2-C8-C9-C10$ $C8-C9-C10-C11$ $C9-C10-C11-C12$ $C9-C10-C11-C12$ $C9-C10-C11-C14$ $C10-C11-C12-C13$ $C14-C11-C12-C13$ $C14-C11-C12-C13$ $C11-C12-C13-C8$ $C9-C8-C13-C12$ $P1-N3-C15-C20$ $P1-N3-C15-C16$ $C20-C15-C16-C17$ $N3-C15-C16-C17$ $C15-C16-C17$ $C15-C16-C19$ $C16-C17-C18-C21$ $C17-C18-C19$ $C16-C17-C18-C20$ $C21-C18-C19-C20$ $C21-C18-C19-C20$ $C16-C15-C20-C19$	$\begin{array}{c} 6.1 (3) \\ -172.26 (15) \\ -1.7 (3) \\ 179.93 (18) \\ 1.1 (3) \\ 0.3 (3) \\ 179.3 (2) \\ -0.9 (3) \\ 180.0 (2) \\ 0.3 (3) \\ 1.0 (3) \\ 179.47 (19) \\ -144.91 (18) \\ 41.9 (3) \\ 41.9 (3) \\ 4.9 (3) \\ 178.1 (2) \\ -3.0 (4) \\ -1.2 (4) \\ -178.0 (2) \\ 3.3 (4) \\ -179.9 (2) \\ -2.8 (3) \end{array}$

C1—C6—C7—N1	143.13 (17)	C18—C19—C20—C15		-1.4 (4)
Hydrogen-bond geometry (Å, °)				
<i>D</i> —Н… <i>A</i>	D—H	H···A	$D \cdots A$	D—H···A
N1—H1N···O2 ⁱ	0.87 (1)	1.92 (1)	2.780 (2)	171.(2)
N2—H2N····O1 ⁱⁱ	0.86 (1)	2.08 (1)	2.886 (2)	156.(2)
N3—H3N…O1 ⁱⁱ	0.86 (1)	2.24 (2)	2.945 (2)	139.(2)
Symmetry codes: (i) – <i>x</i> +1, – <i>y</i> +2, – <i>z</i> +1;	(ii) $-x+2, -y+2, -z+1$.			



